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Functional Advancement of The Mandible in Skeletal Class II Correction with Sliding Plates: A Lateral Cephalometric Study

Muhammad Nasser Sowan*

Abstract

Since early Orthodontics, one of the main concerns is to correct Skeletal Class II. For this Purpose they designed different functional appliances, and performed many cephalometric studies to evaluate treatment results for these appliances on dentofacial complex. Our clinical experience, show the ability of treatment of preadolescents by advancement the mandible in skeletal class II correction with Sliding Plates. and for this purpose, lateral cephalometric study was performed to evaluate treatment results at dentofacial complex. 19 preadolescents ages 11-14 years with skeletal class II and mandibular retrognathism Sliding Plates consist of two separated removable parts, the upper one has midpalatal expansion and vertical wire, the lower is provided with anterior bite plane. The plates were used for 6-12 months. Lateral cephalograms were taken before treatment and immediately after treatment. The results after treatment were compared with the pretreatment measurements before treatment. After treatment, advancement of the mandible and the parts of TMJ has been observed. Thus, the use of sliding plates are useful to correct skeletal class II with mandibular retrognathism, especially in cases associated with narrow upper dental arch for children their ages do not permit the use of pre-functional preparation, and additionally, in cases that require functional rehabilitations.

Key words: sliding plates, skeletal CI II, advancement, function, cephalometric.

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William Roux

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Norman Kingsley

Bite jumping

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Moss

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Pierre Robin

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Harvold

Andresen

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.Robin

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Moss

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Harvold McNamara

Activator

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Andresen

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Bimler

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Martin Schwarz

Activator

Monobloc

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the Double Plate

Functional Approach

Muller Schmuth 1962 -9)

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Hamula

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(11) Muller Schmuth

the Schwarz Double Plate

William Clark's twin block

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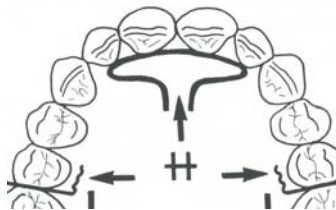
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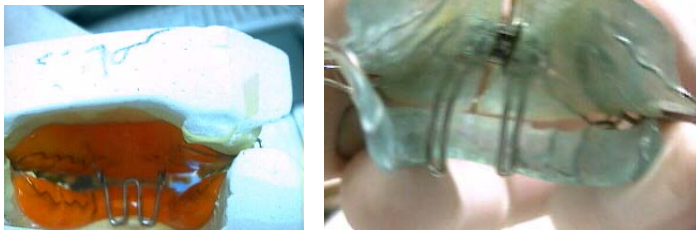
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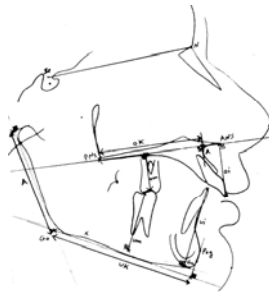
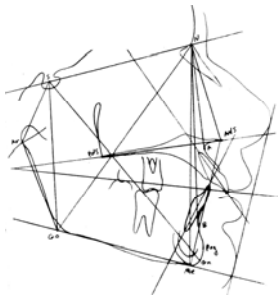
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N-Me		N-ANS/ANS-Me		SN^SPP	
N-ANS		S-Go/N-Me		NS^U.OcP	
ANS-Me		S-N/Go-Me		Go-Me^L.OcP	
S-Go		UK	NSe + 3	NS^GoMe	
S-Ar		OK	2/3 UK	SPP^Go-Me (B)	
Ar-Go		A	5/7 UK	NSAr	
N-S		oi:ui	2/3	SArGo	
Go-Me		om:um	2/3	ArGoMe	
ANS-PNS		oi:om	5/4	Bjork	
		ui:um	5/4	SNA	
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128.7308	122.7692	8.363152	142	117	128.7308	7.685526	115	143	122.7692	N-Me
54.34615	52.80769	3.399661	60	48.5	54.34615	3.250247	47.5	59	52.80769	N-ANS
73.23077	69.57692	5.34094	80	63	73.23077	5.808923	58	77	69.57692	ANS-Me
76.92308	73.38462	7.488453	88	65	76.92308	7.050868	60	85	73.38462	S-Go
34.46154	33.84615	3.275296	40	30.5	34.46154	3.804518	27	38	33.84615	S-Ar
45.11538	42.65385	6.178436	58	35	45.11538	5.249542	32	53	42.65385	Ar-Go
0.736385	0.753077	0.060772	0.85	0.65	0.736385	0.089012	0.6	0.9	0.753077	N-ANS/ANS-Me
59.81538	58.51	5.053356	71.5	51.7	59.81538	7.982134	38.4	72.5	58.51	S-Go/N-Me*100
73.38462	71.80769	4.05254	78	66	73.38462	4.049375	64	77	71.80769	N-S
75.38462	71.61538	5.124101	87	68	75.38462	5.091471	63	83	71.61538	UK
52.15385	51.15385	5.459642	60	42	52.15385	4.947157	38	57	51.15385	OK
3.307692	4.615385	3.939852	12	-3	3.307692	4.537592	-1	12	4.615385	Overbite
24.92308	22.61538	3.569816	31	19	24.92308	2.59931	18	27	22.61538	om
33.61538	31.38462	3.279697	41	30	33.61538	3.379804	28	38	31.38462	um
34.92308	34.84615	2.722179	40	29	34.92308	2.375084	30	38	34.84615	oi

44.30769	43	2.213015	48	41	44.30769	3.674235	38	54	43	Ui
41.15385	40.30769	6.504436	51	29	41.15385	6.365724	26	51	40.30769	NS^GoMe
9.846154	9.038462	3.217042	15.5	6	9.846154	3.287993	5	15	9.038462	SN^SPP
31.61538	31.15385	6.686908	45	16	31.61538	6.75273	15	43	31.15385	SPP^Go-Me (B)
128.2692	128.2308	5.019194	138.5	119	128.2692	5.717719	117	135	128.2308	NSAr
146.5385	144.6923	3.412364	151	140	146.5385	5.850707	137	160	144.6923	SArGo
119.2692	127.3077	27.31957	141	32	119.2692	6.860328	115	139	127.3077	ArGoMe
401.7692	400.3077	7.696361	414	386.5	401.7692	7.261596	385	411	400.3077	Bjork
17.92308	18.34615	7.052914	29	3	17.92308	7.045639	5	29	18.34615	NS^U.OcP
18.73077	19.53846	7.21288	30	10	18.73077	6.792954	10	30.5	19.53846	Go-Me^L.OcP
77.73077	78.03846	3.816714	85	72	77.73077	3.721903	73	85	78.03846	SNA
73.23077	72.65385	2.862221	78	69	73.23077	3.242842	67.5	79	72.65385	SNB
4.423077	5.384615	2.225292	10	2	4.423077	1.769579	2	8	5.384615	ANB
74	64.92308	12.33559	101	59	74	5.866026	56	77	64.92308	U1^SpP
101.5385	97.30769	7.731056	120	91	101.5385	7.250111	87	110	97.30769	L1^Go-Me
128.7308	122.7692	8.363152	142	117	128.7308	7.685526	115	143	122.7692	N-Me

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2.32	2.13	8.36	7.69	128.73	122.77	N-Me
0.94	0.90	3.40	3.25	54.35	52.81	N-ANS
1.48	1.61	5.34	5.81	73.23	69.58	ANS-Me
2.08	1.96	7.49	7.05	76.92	73.38	S-Go
0.91	1.06	3.28	3.80	34.46	33.85	S-Ar
1.71	1.46	6.18	5.25	45.12	42.65	Ar-Go
0.02	0.02	0.06	0.09	0.74	0.75	N-ANS/ANS-Me
1.40	2.21	5.05	7.98	59.82	58.51	S-Go/N-Me*100
1.12	1.12	4.05	4.05	73.38	71.81	N-S
1.42	1.41	5.12	5.09	75.38	71.62	Go-Me
1.51	1.37	5.46	4.95	52.15	51.15	ANS-PNS
1.09	1.26	3.94	4.54	3.31	4.62	Overbite
0.99	0.72	3.57	2.60	24.92	22.62	U6/SPP
0.91	0.94	3.28	3.38	33.62	31.38	L6/Go-Me
0.75	0.66	2.72	2.38	34.92	34.85	U1/SPP
0.61	1.02	2.21	3.67	44.31	43.00	L1/GoMe
1.80	1.77	6.50	6.37	41.15	40.31	SN/Go-Me
0.89	0.91	3.22	3.29	9.85	9.04	Sn/SPP
1.85	1.87	6.69	6.75	31.62	31.15	SPP/GoMe
1.39	1.59	5.02	5.72	128.27	128.23	NSAr
0.95	1.62	3.41	5.85	146.54	144.69	SArGo
7.58	1.90	27.32	6.86	119.27	127.31	ArGoMe
2.13	2.01	7.70	7.26	401.77	400.31	Bjork
1.96	1.95	7.05	7.05	17.92	18.35	SN/U.OCC.Plane
2.00	1.88	7.21	6.79	18.73	19.54	GoMe/L.occ.Plane
1.06	1.03	3.82	3.72	77.73	78.04	SNA
2.86	3.24	73.23	72.65	13	13	SNB
2.23	1.77	4.42	5.38	13	13	ANB
12.34	5.87	74.00	64.92	13	13	U1/SPP
7.73	7.25	101.54	97.31	13	13	L1/GoMe

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	0.002	12	3.85	1.55	5.58	5.96	<i>N-Me</i>
	0.028	12	2.50	0.62	2.22	1.54	<i>N-ANS</i>
	0.000	12	6.23	0.59	2.12	3.65	<i>ANS-Me</i>
	0.001	12	4.32	0.82	2.95	3.54	<i>S-Go</i>
	0.319	12	1.04	0.59	2.13	0.62	<i>S-Ar</i>
	0.0101	12	3.05	0.81	2.91	2.46	<i>Ar-Go</i>
	0.144	12	-1.56	0.01	0.04	-0.02	<i>N-ANS/ANS-Me</i>
	0.406	12	0.86	1.51	5.46	1.31	<i>S-Go/N-Me*100</i>
	0.046	12	2.23	0.71	2.55	1.58	<i>N-S</i>
	0.004	12	3.53	1.07	3.85	3.77	<i>Go-Me</i>
	0.284	12	1.12	0.89	3.21	1.00	<i>ANS-PNS</i>
	0.141	12	-1.58	0.83	2.99	-1.31	<i>Overbite</i>
	0.003	12	3.76	0.61	2.21	2.31	<i>U6/SPP</i>
	0.001	12	4.62	0.48	1.74	2.23	<i>L6/Go-Me</i>
	0.897	12	0.13	0.58	2.10	0.08	<i>U1/SPP</i>
	0.222	12	1.29	1.02	3.66	1.31	<i>L1/GoMe</i>
	0.237	12	1.24	0.68	2.45	0.85	<i>SN/Go-Me</i>
	0.089	12	1.85	0.44	1.58	0.81	<i>Sn/SPP</i>
	0.593	12	0.55	0.84	3.03	0.46	<i>SPP/GoMe</i>
	0.968	12	0.04	0.93	3.36	0.04	<i>NSAr</i>
	0.231	12	1.26	1.46	5.28	1.85	<i>SArGo</i>
	0.328	12	-1.02	7.88	28.40	-8.04	<i>ArGoMe</i>
	0.013	12	2.90	0.50	1.82	1.46	<i>Bjork</i>
	0.536	12	-0.64	0.66	2.40	-0.42	<i>SN/U.OCC.Plane</i>
	0.309	12	-1.06	0.76	2.74	-0.81	<i>GoMe/L.occ.Plane</i>
	0.606	12	-0.53	0.58	2.10	-0.31	<i>SNA</i>
	0.082	12	1.90	0.30	1.10	0.58	<i>SNB</i>
	0.048	12	-2.20	0.44	1.57	-0.96	<i>ANB</i>
	0.015	12	2.85	3.19	11.49	9.08	<i>U1/SPP</i>
	0.001	12	4.46	0.95	3.42	4.23	<i>L1/GoMe</i>

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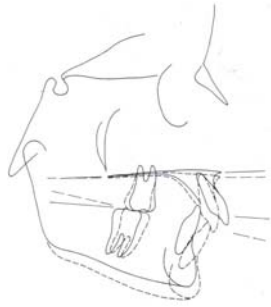
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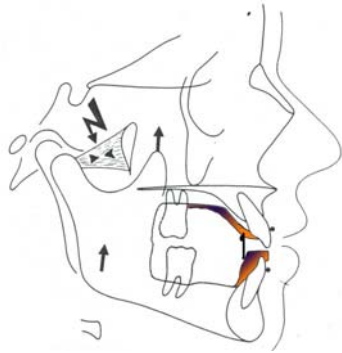
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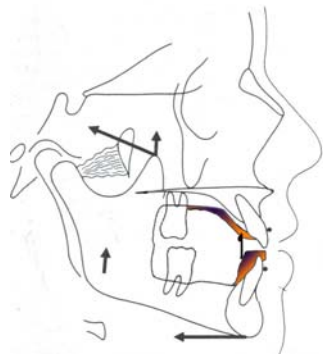
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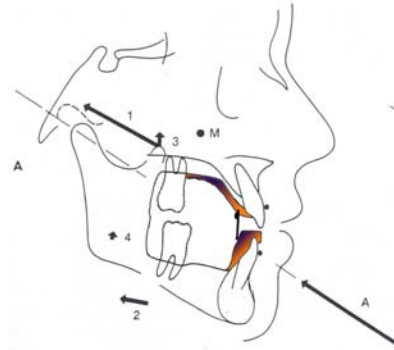
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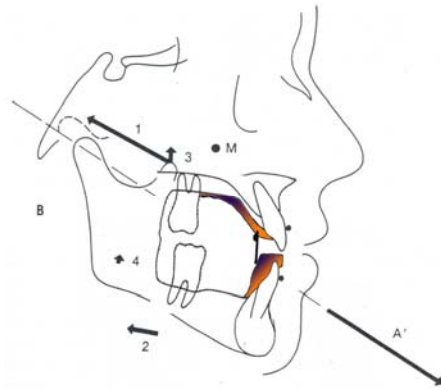
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